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| Hilman F PardedeNational Research and Innovation Agency of IndonesiaIndonesiaShashikant S. PatilMumbai UniversityIndiaTeguh PrakosoDiponegoro UniversityIndonesiaRicardus Anggi PramunendarUniversitas Dian NuswantoroIndonesiaEra PurwantoElectronic Engineering Polytechnic Institute Of SurabayaIndonesiaHarikumar RajaguruBanari Amman Institute of TechnologyIndiaGrienggrai RajchakitMaejo UniversityThailandPriya RanjanBhuvaneshvar Institute of TechnologyIndiaSirimonpak SKMUTTThailandArshad SalihLect.IraqIvan SetyawanSatya Wacana Christian UniversityIndonesiaNathere A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudhongkhongNational Tsing Hua UniversityIndonesiaNational Tsing Hua UniversityIndonesiaIndonesiaNico SurathaBina Nusantara UniversityIndonesiaSuherman SuhermanNational Tsing Hua UniversityIndonesiaNico SurathaBina Nusantara UniversityIndonesiaNico SurathaBina Nusantara UniversityIndonesiaNico SurathaBina Nusantara UniversityIndonesiaNico SurathaBina Nusantara Unive | | Instituto Politécnico Nacional | Mexico |
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| Teguh PrakosoDiponegoro UniversityIndonesiaRicardus Anggi PramunendarUniversitas Dian NuswantoroIndonesiaEra PurwantoElectronic Engineering Polytechnic Institute Of SurabayaIndonesiaHarikumar RajaguruBannari Amman Institute of TechnologyIndiaGrienggrai RajchakitMaejo UniversityThailandPriya RanjanBhuvaneshvar Institute of TechnologyIndiaSirimonpak SKMUTTThailandArshad SalihLect.IraqIwan SetyawanSatya Wacana Christian UniversityIndonesiaNadheer A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University, VadodaraIndonesiaHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNational Tsing Hua UniversityIndonesiaKuugaruthaBina Nusantara UniversityIndonesiaSuderong KongSina Nusantara UniversityIndonesiaSutersita Sumatera UniversityIndonesiaSutersita Sumatera UniversityIndonesiaSutersita Sumatera UniversityIndonesiaSutersita Sumatera UniversityIndonesiaSutersita Sumatera UniversityIndonesiaSutersita Sumatera UniversityIndonesiaNational Rese | Hilman F Pardede | National Research and Innovation Agency of Indonesia | Indonesia |
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| Era PurwantoSurabayaIndonesiaHarikumar RajaguruBannari Amman Institute of TechnologyIndiaGrienggrai RajchakitMaejo UniversityThailandPriya RanjanBhuvaneshvar Institute of TechnologyIndiaSirimonpak SKMUTTThailandArshad SalihLect.IraqIwan SetyawanSatya Wacana Christian UniversityIndonesiaNadheer A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University, VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaOdugandUniversity of the AssumptionPhilippinesChudanat Sutherman SuhermaUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityIndonesiaNatio SuranthaBina Nusantara UniversityIndonesiaSutherman SuhermaUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNational Tsing Hua UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityI | | Universitas Dian Nuswantoro | Indonesia |
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| Sirimonpak SKMUTTThailandArshad SalihLect.IraqIwan SetyawanSatya Wacana Christian UniversityIndonesiaNadheer A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University, VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongMuTTIndonesiaSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Grienggrai Rajchakit | Maejo University | Thailand |
| Arshad SalihLect.IraqIwan SetyawanSatya Wacana Christian UniversityIndonesiaNadheer A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University, VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Priya Ranjan | Bhuvaneshvar Institute of Technology | India |
| Iwan SetyawanSatya Wacana Christian UniversityIndonesiaNadheer A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University, VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Sirimonpak S | KMUTT | Thailand |
| Nadheer A. ShalashAl-Mamoon University CollegeIraqAditi SharmaParul University, VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaWiwin SuwarningsihNational Research and Innovation Agency (BRIN)IndonesiaGeorge TambouratzisInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Arshad Salih | Lect. | Iraq |
| Aditi SharmaParul University, VadodaraIndiaFatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaNico SuranthaInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItaly | Iwan Setyawan | Satya Wacana Christian University | Indonesia |
| Fatina ShukurUniversity of KufaIraqHarco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaWiwin SuwarningsihNational Research and Innovation Agency (BRIN)IndonesiaGeorge TambouratzisInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Nadheer A. Shalash | Al-Mamoon University College | Iraq |
| Harco Leslie Hendric Spits WarnarsBina Nusantara UniversityIndonesiaJoey SubaUniversity of the AssumptionPhilippinesChudanat SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaWiwin SuwarningsihNational Research and Innovation Agency (BRIN)IndonesiaGeorge TambouratziInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItaly | Aditi Sharma | Parul University, Vadodara | India |
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| SudthongkhongKMUTTThailandSuherman SuhermanUniversitas Sumatera UtaraIndonesiaHung-Min SunNational Tsing Hua UniversityTaiwanAndi SunyotoUniversitas Amikom YogyakartaIndonesiaNico SuranthaBina Nusantara UniversityIndonesiaWiwin SuwarningsihNational Research and Innovation Agency (BRIN)IndonesiaGeorge TambouratzisInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Joey Suba | University of the Assumption | Philippines |
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| Nico SuranthaBina Nusantara UniversityIndonesiaWiwin SuwarningsihNational Research and Innovation Agency (BRIN)IndonesiaGeorge TambouratzisInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Hung-Min Sun | National Tsing Hua University | Taiwan |
| Wiwin SuwarningsihNational Research and Innovation Agency (BRIN)IndonesiaGeorge TambouratzisInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Andi Sunyoto | Universitas Amikom Yogyakarta | Indonesia |
| George TambouratzisInstitute for Language & Speech ProcessingGreeceAlessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Nico Surantha | Bina Nusantara University | Indonesia |
| Alessandro TestaMinistry of Economy and FinanceItalyHapnes TobaMaranatha Christian UniversityIndonesia | Wiwin Suwarningsih | National Research and Innovation Agency (BRIN) | Indonesia |
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| Zhe Zhang | Aerospace Information Research Institute, Chinese Academy of Sciences | China |

TOC

2022 9th International Conference on Electrical Engineering, Computer Science and Informatics (EECSI)

| Experimental Convolutional-Recurrent Network in ECG Rhythm for Atrial Fibrillation Classification | |
|--|----|
| Annisa Darmawahyuni (University of Sriwijaya, Indonesia), Bambang Tutuko (Intelligent System Research Group Computer | |
| Science Faculty Universitas Sriwijaya Indonesia, Indonesia), Muhammad Naufal Rachmatullah (Universitas Sriwijaya, Indonesia), | |
| Siti Nurmaini (University of Sriwijaya, Indonesia), Firdaus Firdaus (Universitas Sriwijaya, Indonesia) | |
| Comparison of Machine Learning Performance for Covid-19 X-ray Image Classification Based on Texture Features | |
| Yessi Jusman (Universitas Muhammadiyah Yogyakarta, Indonesia), Wikan Tyassari (University of Muhammadiyah Yogyakarta, | |
| Indonesia), Ibnu Rahmat Siddik (Universitas Muhammadiyah Yogyakarta, Indonesia), Rika Nursanthika (Universitas | |
| Muhammadiyah Yogyakarta, Indonesia), Veby Yuly Sherly (Universitas Muhammadiyah Yogyakarta, Indonesia) | 7 |
| Natural language Processing and Ontology based Decision Support System for Diabetic Patients | |
| Ritesh Chandra (Indian Institute of Information Technology Allahabad, India), Sadhana Tiwari (Indian Institute of Information | |
| Technology Allahabad, India), Abhaya Shukla (Manipal Institute of Technology, India), Sonali Agarwal (Indian Institute of | |
| Information Technology, Allahabad, India), Muhammad Syafrullah (Universitas Budi Luhur, Indonesia), Krisna Adiyarta | |
| (Universitas Budi Luhur, Indonesia) | |
| Time and Frequency Domain Feature Selection Using Mutual Information for EEG-based Emotion Recognition | |
| Adhi Dharma Wibawa (Institut Teknologi Sepuluh Nopember, Indonesia), Nur Fatih (Institut Teknologi Sepuluh Nopember, | |
| Indonesia), Yuri Pamungkas (ITS Surabaya, Indonesia), Monica Pratiwi (Institut Teknologi Sepuluh Nopember, Indonesia, | |
| Indonesia), Prio Adi Ramadhani (Institut Teknologi Sepuluh Nopember, Indonesia), Suwadi Suwadi (Institut Teknologi Sepuluh | |
| Nopember, Indonesia, Indonesia) | |
| Evaluation of Gated-Recurrent Unit for Estimating Finger-Joint Angle using Surface Electromyography Signal | |
| Zamroni Ilyas (University of Jember, Indonesia), Khairul Anam (University of Jember, Indonesia), Widjonarko Widjonarko | |
| (Universitas Jember, Indonesia), Cries Avian (National Taiwan University of Science and Technology, Taiwan), Aris Zainul | |
| Muttaqin (University of Jember, Indonesia), Mochamad Edoward Ramadhan (Ramadhan, Indonesia) | 25 |
| Classification of Covid-19 Variants Using Boosting Algorithm | |
| Izzudin Muhammad (Institut Teknologi Sepuluh Nopember, Indonesia), Imam Mukhlash (Institut Teknologi Sepuluh Nopember | |
| Surabaya, Indonesia), Mohammad Jamhuri (Institut Teknologi Sepuluh Nopember, Indonesia), Mohammad Iqbal (Institut | |
| Teknologi Sepuluh Nopember, Indonesia), Mohammad Isa Irawan (Institut Teknologi Sepuluh Nopember, Indonesia) | |
| Anomaly detection on MNIST stroke simulation dataset | |
| Ojas Vishwakarma (IIIT Allahabad, India), Sonali Agarwal (Indian Institute of Information Technology, Allahabad, India), Soundra | |
| Pandian (Ministry of Electronics and Information Technology New Delhi India, India), Muhammad Syafrullah (Universitas Budi | |
| Luhur, Indonesia), Krisna Adiyarta (Universitas Budi Luhur, Indonesia), Sanjay Kumar Sonbhadra (Siksha O Anusandhan | |
| Bhubaneswar India, India) | |
| Detection of Fetal Cardiac Chamber Three Vessel Trachea View using Deep Learning | |
| Ade Sapitri (Universitas Sriwjaya, Indonesia) | |
| Support Vector Machine Method for Predicting Children's Emotions | |
| Fildzah Aure Gehara Zhafirah (Electronic Engineering Polytechnic Institute of Surabaya, Indonesia), Rika Rokhana (Politeknik | |
| Elektronika Negeri Surabaya & Institut Teknologi Sepuluh Nopember, Indonesia) | |
| Decision Support System using Weighting Similarity Model for Constructing Ground-Truth Dataset | |
| M. Miftakul Amin (Politeknik Negeri Sriwijaya, Indonesia), Deris Stiawan (University of Sriwijaya, Indonesia), Ermatita Ermatita | |
| (Sriwijaya University & Computer Science Faculty, Indonesia), Imam Much Ibnu Subroto (Universitas Islam Sultan Agung, | |
| Indonesia), Lukman Lukman (Directorat General of Higher Education Research and Technology, Indonesia) | |

| Comparison Of Naive Bayes And Support Vector Machine For Detecting Hoax In Indonesian Tweet Case Study Of Tweet Covid-19 | |
|--|----|
| Indra Indra (Universitas Budi Luhur, Indonesia), Suci Setiawati (Universitas Budi Luhur, Indonesia), Sukha Vaddhana (Universitas | |
| Budi Luhur, Indonesia), Anindita Septiarini (Universitas Mulawarman, Indonesia) | |
| Pot Detection System Using YOLO | |
| Adlian Jefiza (Politeknik Negeri Batam, Indonesia), Muhammad Zainuddin Lubis (Politeknik Negeri Batam, Indonesia), Diono Diono (Politeknik Negeri Batam, Indonesia), Ahmad Maulana Prabu (Politeknik Negeri Batam, Indonesia) | 67 |
| Comparative Study Of Convolutional Neural Network And Haar Cascade Performance On Mask Detection Systems Using Matlab | |
| Faisal Ali Mahaputra (Mercu Buana University, Indonesia), Imelda Simanjuntak (Universitas Mercu Buana, Indonesia), Yuliza | |
| Yuliza Yuliza (University of Mercu Buana, Indonesia), Heryanto Heryanto (Universitas Pertahanan, Indonesia), Agus Rochendi | |
| (Badan Riset dan Inovasi Nasional, Indonesia), Lukman Silalahi (Universitas Mercu Buana, Indonesia) | |
| Cyberattack Feature Selection using Correlation-Based Feature Selection Method in an Intrusion Detection System | |
| Deris Stiawan (University of Sriwijaya, Indonesia), Ahmad Heryanto (Sriwijaya University, Indonesia), Mohd. Yazid Idris (Universiti | |
| Teknologi Malaysia, Malaysia), Rahmat Budiarto (Al Baha University, Saudi Arabia) | |
| Market Basket Analysis Using FP-Growth Algorithm On Retail Sales Data | |
| Muhammad Raihan Pradana (Universitas Budi Luhur, Indonesia), Muhammad Syafrullah (Universitas Budi Luhur, Indonesia), | |
| Hendri Irawan (Universitas Budi Luhur, Indonesia), Irawan Irawan (Universitas Budi Luhur, Indonesia), Joko Christian Chandra | |
| (Universitas Budi Luhur, Indonesia), Achmad Solichin (Universitas Budi Luhur, Indonesia) | |
| | |

| Optimizing SVM Hyperparameters using Predatory Swarms Algorithms for Use Case Points Estimation | |
|---|------|
| Ardiansyah Ardiansyah (Universitas Ahmad Dahlan, Indonesia), Ridi Ferdiana (Universitas Gadjah Mada, Indonesia), Adhistya | |
| Erna Permanasari (Universitas Gadjah Mada, Indonesia) | |
| A dynamic task scheduling model for mobile cloud computing | |
| Zahraa A. Jaaz (Universiti Tenaga Nasional (UNITEN), Malaysia), Shaymaa Adnan Abdulrahman (Imam Jaafer Alsadiq & Ain | |
| shams, Iraq), Hanaa M. Mushgil (AlNahrain University, Iraq) | |
| Author Classification on Bibliographic Data Using Capsule Networks Architecture | |
| Firdaus Firdaus (Universitas Sriwijaya, Indonesia), Wais Alqarni (Intelligent System Research Group, Indonesia), Siti Nurmaini | |
| (University of Sriwijaya, Indonesia), Annisa Darmawahyuni (University of Sriwijaya, Indonesia), Ade Sapitri (Universitas Sriwijaya, | |
| Indonesia), Muhammad Naufal Rachmatullah (Universitas Sriwijaya, Indonesia), Suci Dwi Lestari (Universitas Sriwijaya, | 1.01 |
| Indonesia) | 101 |
| Improving the Accuracy of Text Classification Using the Over Sampling Technique in the Case of Sinovac Vaccine | |
| Muhammad Rizky Pribadi (Universitas Multi Data Palembang, Indonesia), Hindriyanto D Purnomo (Satya Wacana Christian University, Indonesia), Hendry Hendry (Chaoyang University of Technology & Satya Wacana Christian University, Taiwan), | |
| Kristoko Dwi Hartomo (Universitas Kristen Satya Wacana, Indonesia), Irwan Sembiring (Universitas Kristen Satya Wacana | |
| Salatiga, Indonesia), Ade Iriani (Satya Wacana Christian University, Indonesia). | 106 |
| Prediction of Non-Performing Loans For Credit Application Analysis of Rural Bank Using Random Forest | |
| Mutiara Annisa (Universitas Budi Luhur, Indonesia), Rusdah Rusdah (Universitas Budi Luhur, Indonesia) | 111 |
| Data Fusion for Predictive Maintenance of Industrial Assets Using Digital Twin | |
| Christian Avornu (Huzhou University, China) | |
| Best Lecturer Decision Support System Using Method Analytical Hierarchy Process (AHP) and Method SAW | 113 |
| Nurhayati Nur Nurhayati (Universitas Budi Luhur, Indonesia), Dwi Pebrianti (International Islamic University Malaysia, Malaysia), | |
| Luhur Bayuaji (UMP, Malaysia), Muhammad Syafrullah (Universitas Budi Luhur, Indonesia) | 122 |
| Implementation of LSSVM in Classification of Software Defect Prediction Data with Feature Selection | |
| Thingkilia Finnatia Husin (Universitas Multi Data Palembang, Indonesia), Muhammad Rizky Pribadi (Universitas Multi Data | |
| Palembang, Indonesia), Yohannes Yohannes (Universitas Multi Data Palembang, Indonesia) | 126 |
| Research on optimization strategy of medical data information security and privacy | |
| Haider Abdulshaheed (Baghdad College, Iraq), Sura Abdulmunem Mohammed Al-Juboori (Ministry of Higher Education and | |
| Scientific Research, Iraq), Intisar A.M Al-Sayed (Ashur University College, Iraq), Israa Al Barazanchi (College of Computing and | |
| Informatics & Universiti Tenaga Nasional (UNITEN), Malaysia), Hassan Muwafaq Gheni (Al Mustaqbal University College & | |
| Babylon University Collage of Engineering, Iraq), Zahraa A. Jaaz (Universiti Tenaga Nasional (UNITEN), Malaysia) | 132 |

| | redicting Risk Matrix in Software Development Projects using BERT and K-Means | |
|----------------|--|------------|
| | Marzuki Pilliang (Esa Unggul, Indonesia), Munawar Munawar (Esa Unggul University, Indonesia), Muhammad Hadi (Esa Unggul | |
| | University, Indonesia), Gerry Firmansyah (Esa Unggul University, Indonesia), Budi Tjahjono (Esa Unggul University, Indonesia) | 137 |
| D | evelopment of Knowledge Management System with Soft System Metodhology in Aquatic Organization | |
| | Anugerah Widi (University of Multi Data Palembang, Indonesia), Eko Sediyono (Universitas Kristen Satya Wacana, Indonesia), | |
| | Kristoko Dwi Hartomo (Universitas Kristen Satya Wacana, Indonesia), Irwan Sembiring (Universitas Kristen Satya Wacana | |
| | Salatiga, Indonesia), Ade Iriani (Satya Wacana Christian University, Indonesia), Hendry Hendry (Chaoyang University of | |
| | Technology & Satya Wacana Christian University, Taiwan) | 143 |
| A | n Information Security Policy Development Process in Higher Education Institution: A Case Study | |
| | Wan Basri Wan Ismail (Management& Science University, Malaysia), Setyawan Widyarto (Universiti Selangor, Malaysia), Krisna | |
| | Adiyarta (Universitas Budi Luhur, Indonesia), Muhammad Syafrullah (Universitas Budi Luhur, Indonesia), Laili Mardziah Tajuddin | |
| | (Universiti Selangor, Malaysia) | 147 |
| | Optimization of Sentiment Analysis using Naïve Bayes with Features Selection Chi-Square and Information Gain or Accuracy Improvement | |
| | Denni Kurniawan (Universitas Budi Luhur, Indonesia) | 153 |
| H | lybrid Method for Churn Prediction Model in The Case of Telecommunication Companies | |
| | Dwi Pebrianti (International Islamic University Malaysia, Malaysia), Desti Destiansari Istinabiyah (Budi Luhur University, | |
| | Indonesia), Luhur Bayuaji (FSKPP, Universiti Malaysia Pahang, Malaysia), Rusdah Rusdah (Universitas Budi Luhur, Indonesia) | 161 |
| Ai O, fo | Anugerah Widi (University of Multi Data Palembang, Indonesia), Eko Sediyono (Universitas Kristen Satya Wacana, Indonesia), Kristoko Dwi Hartomo (Universitas Kristen Satya Wacana, Indonesia), Irwan Sembiring (Universitas Kristen Satya Wacana Salatiga, Indonesia), Ade Iriani (Satya Wacana Christian University, Indonesia), Hendry Hendry (Chaoyang University of Technology & Satya Wacana Christian University, Taiwan) In Information Security Policy Development Process in Higher Education Institution: A Case Study Wan Basri Wan Ismail (Management& Science University, Malaysia), Setyawan Widyarto (Universiti Selangor, Malaysia), Krisna Adiyarta (Universitas Budi Luhur, Indonesia), Muhammad Syafrullah (Universitas Budi Luhur, Indonesia), Laili Mardziah Tajuddin (Universiti Selangor, Malaysia) Deptimization of Sentiment Analysis using Naïve Bayes with Features Selection Chi-Square and Information Gain for Accuracy Improvement Denni Kurniawan (Universitas Budi Luhur, Indonesia) Lybrid Method for Churn Prediction Model in The Case of Telecommunication Companies Dwi Pebrianti (International Islamic University Malaysia, Malaysia), Desti Destiansari Istinabiyah (Budi Luhur University, | 147 153 |

| Intelligent Sentiment Analysis on Cellphone Checking by Police Officer | |
|--|-----|
| Barep Prasetyo (Indonesia), Yaya Sudarya Triana (University of Mercu Buana, Indonesia), Rahmat Budiarto (Al Baha University, | |
| Saudi Arabia), Deris Stiawan (University of Sriwijaya, Indonesia) | 167 |
| Fuzzy Cognitive Maps for Intelligent Agent's Artificial Situational Awareness in Collaborative Driving Context | |
| Rinta Kridalukmana (Diponegoro University, Indonesia), Dania Eridani (Diponegoro University, Indonesia), Risma Septiana | |
| (Diponegoro University, Indonesia), Adian Fatchur Rochim (Diponegoro University, Indonesia), Charisma Setyobudhi | |
| (Diponegoro University, Indonesia) | 173 |
| Monitoring System of Natural Disaster from Twitter Messages Using Support Vector Machine | |
| Casi Setianingsih (Telkom University, Indonesia) | 179 |
| Forecasting indoor temperature for smart buildings with ARIMA, SARIMAX, and LSTM: A fusion approach | |
| Shashi Shekhar Kumar (Indian Institute of Information Technology Allahabad, India), Ashutosh Kumar (Indian Institute of | |
| Information Technology Allahabad, India), Sonali Agarwal (Indian Institute of Information Technology, Allahabad, India), | |
| Muhammad Syafrullah (Universitas Budi Luhur, Indonesia), Krisna Adiyarta (Universitas Budi Luhur, Indonesia) | 186 |
| User Satisfaction Analysis of PeduliLindungi Application Using End User Computing Satisfaction (EUCS) Method | |
| Ahmad Reza Yudistira (Telkom University, Indonesia), Hilal H. Nuha (Telkom University, Indonesia), Kusuma Adi Achmad | |
| (Telkom University & City Government of Pekalongan, Indonesia) | 193 |
| The Analysis of Readiness and Acceptance of Learning Management System (LMS) Usage in Universities of East Java | |
| Fahrobby Adnan (University of Jember, Indonesia), Maulida Dwi Agustiningsih (KH Achmad Siddiq State Islamic University, | |
| Indonesia), Lutfi Ariefianto (University of Jember, Indonesia) | 198 |
| Utilization of Smart Greenhouse to Increase Chrysanthemum Growth in the Vegetative Phase by Monitoring Using Firebase | |
| Muhammad Tito Maiza Henanda (Telkom University, Indonesia), Hilal H. Nuha (Telkom University, Indonesia), Endro Ariyanto | |
| (Telkom University, Indonesia) | 204 |
| Smart Attendance for Lecture with Physical Distancing Based on The Internet of Things (IoT) | |
| Nur Fauzan Jundi Rabbany (Telkom University, Indonesia), Hilal H. Nuha (Telkom University, Indonesia), Muhammad Johan | |
| Alibasa (Telkom University, Indonesia) | 210 |
| Combining Dynamic K-Means and Binary Search Centroid to Optimize Clustering Results on Home Industry Datasets | |
| Hadi Santoso (ISB Atma Luhur, Indonesia), Hilyah Magdalena (ISB Atma Luhur, Indonesia) | 215 |
| | |

| Comparison of Anomaly Based and Signature Based Methods in Detection of Scanning Vulnerability | |
|---|-----|
| Ismail Puji Saputra (Universitas Muhammadiyah Metro & Universitas Amikom Yogyakarta, Indonesia), Ema Utami (Universitas | |
| Amikom Yogyakarta, Indonesia), Alva Muhammad (Universitas Amikom Yogyakarta, Indonesia) | 221 |
| Feature Selection using Chi Square to Improve Attack Detection Classification in IoT Network: Work in Progress | |
| Zulhipni Reno Saputra Elsi (Univeritas Sriwijaya & Univeritas Muhamadiyah Palembang, Indonesia), Deris Stiawan (University of | |
| Sriwijaya, Indonesia), Ahmad Fali Oklilas (Faculty of Computer Science, Universitas Sriwijaya, Indonesia), Susanto Susanto | |
| (Sriwijaya University & Universitas Bina Insan, Indonesia), Kurniabudi Kurniabudi (STIKOM Dinamika Bangsa, Indonesia), Yesi | |
| Novaria Kunang (Universitas Sriwijaya & Universitas Bina Darma, Indonesia), Mohd. Yazid Idris (Universiti Teknologi Malaysia, | |
| Malaysia), Rahmat Budiarto (Al Baha University, Saudi Arabia) | 226 |
| Implementation of the Affine Segmentation Point Method and Image Blending Techniques in Creating New Songket Motifs | |
| Agung Ramadhanu (Universitas Putra Indonesia YPTK Padang, Indonesia), Jufriadif Na`am (Universitas Putra Indonesia YPTK | |
| Padang, Indonesia), Gunadi Widi Nurcahyo (Universitas Putera Indonesia YPTK Padang, Indonesia), Yuhandri Yunus (Universitas | |
| Putra Indonesia YPTK Padang, Indonesia) | 233 |
| Auto-Generating Business Process Model From Heterogeneous Documents: A Comprehensive Literature Survey | |
| Uce Indahyanti, UI (Institut Teknologi Sepuluh Nopember Surabaya & Universitas Muhammadiyah Sidoarjo, Indonesia), Arif | |
| Djunaidy (Institut Teknologi Sepuluh Nopember, Indonesia), Daniel Siahaan (Institut teknologi Sepuluh Nopember, Indonesia) | 239 |
| Usability Analysis of My TelU Application Using System Usability Scale | |
| Fajar Angga Sigalingging (Telkom University & Telkom Indonesia, Indonesia), Muhammad Johan Alibasa (Telkom University, | |
| Indonesia), Hilal H. Nuha (Telkom University, Indonesia) | 244 |
| E-counseling-based Expressive Writing Therapy Platform for Overcoming Student Mental Health Problems | |
| Tifanny Nabarian (Nurul Fikri College of Technology, Indonesia), Yekti Wirani (Nurul Fikri College of Technology, Indonesia), | |
| Miftahussaadah Putri Siddiq (Nurul Fikri College of Technology, Indonesia), Aseptianova Aseptianova (University of | |
| Muhammadiyah Palembang, Indonesia), M. Zalili Aziz (University of Muhammadiyah Palembang, Indonesia), Ananto Dwi | |
| Saputro (Badan Siber dan Sandi Negara, Indonesia) | 250 |
| | |

| Multi-Criteria Decision-Making Method for Supplier Selection in Transformer Production | |
|---|-----|
| Utku Balcı (Galatasaray University, Turkey) | 256 |
| Analysis of Starting Current And Electrical Energy In Three Phase Induction Motor As A Chemical Processing System In. PT RIAU ANDALAN PULP & PAPER | |
| Fadhli Palaha (Sekolah Tinggi Teknologi Pekanbaru, Indonesia), Yolnasdi Yol (Sekolah Tinggi Teknologi Pekanbaru, Indonesia), Ermawati Erma (Sekolah Tinggi Teknologi Pekanbaru, Indonesia), Engla Harda Arya (Sekolah Tinggi Teknologi Pekanbaru, Indonesia), Machda Machadalena (Sekolah Tinggi Teknologi Pekanbaru, Indonesia), Eki Ki Rinal (Sekolah Tinggi Teknologi Pekanbaru, Indonesia) | 264 |
| Design and Implementation of an Internet of Things Based Smart Energy Meter using Radio Frequency communication protocol | |
| Ahmed Ibrahim Elkassar (Arab Academy for Science and Technology, Egypt), Eman Hamdan (Arab Academy for Science and Technology, Egypt), Walid A.M. Ghoniem (Arab Academy for Science and Technology, Egypt), Ahmed Abouelfarag (Arab Academy for Science and Technology, Egypt) | 270 |
| Construction of Slow and Fast Field Antenna for Detecting Lightning Strikes in South Sumatera | |
| <mark>Wiwin Armoldo Oktaviani</mark> (Universitas Sriwijaya, Indonesia), Muhammad Abu Bakar Sidik (Faculty of Engineering, Universitas Sriwijaya Ogan Ilir, Indonesia), Mohd Riduan Ahmad (Universiti Teknikal Malaysia Melaka, Malaysia), Muhammad Irfan Jambak (Universitas Sriwijaya, Indonesia), Rio Yusdizali (Universitas Sriwijaya, Indonesia) | 276 |
| Preliminary Analysis on State Vector and Computational Time of Dynamic State Estimation | |
| Nurul Fauzana Imran Gulcharan (Universiti Teknologi Petronas, Malaysia), Hanita Daud (Universiti Teknologi PETRONAS, Malaysia), Nursyarizal Bin Mohd Nor (Universiti Teknologi Petronas, Malaysia), Taib Ibrahim (Malaysia) | 283 |
| Identification of impedance changes in metal using RFID RC522 based on arduino uno | |
| Vector Pratomo (Universitas Pancasila, Indonesia), Wisnu Broto (Universitas Pancasila, Indonesia), Gunady Haryanto, GH (University of Pancasila, Indonesia), Untung Priyanto (Pancasila University, Indonesia) | 288 |
| | |

| Deep Learning Neural Networks Diagnosis of Power Transformer through Its DGA Data | |
|--|-----|
| Hansel Matthew (Universitas Indonesia, Indonesia), Aqila Dzikra Ayu (Universitas Indonesia, Indonesia), Iman Herlambang | |
| Suherman (Universitas Indonesia, Indonesia), Aries Subiantoro (Universitas Indonesia, Indonesia), Benyamin Kusumoputro | |
| (Universitas Indonesia, Indonesia) | 292 |
| Simulation of D-shaped Optical Fiber Sensor for Adulterant Traces in Liquid Petrochemical | |
| Najwa Azzahari (Universiti Teknologi Malaysia, Malaysia), Husni Hani Jameela Sapingi (Laser Center, Universiti Teknologi | |
| Malaysia, Malaysia) | 297 |
| Control and Monitoring System Design Tunnel Light Using NodeMCU and Arduino Nano and networking | |
| Albert Gifson Hutajulu (ITPLN, Indonesia), Juara Mangapul Tambunan (ITPLN, Indonesia), Hendrianto Husada (INSTITUT | |
| TEKNOLOGI PLN Jakarta, Indonesia), Yani Prabowo (Computer Science & Universitas Budi Luhur, Indonesia) | 301 |
| IoT-Based Smart Parking Management System Using ESP32 Microcontroller | |
| Joni W. Simatupang (President University, Indonesia & NTUST, Taiwan), Aida Mahdalena Lubis (President University, Indonesia), | |
| Vincent Vincent (Institut Teknologi Bandung, Indonesia) | 305 |
| Lamp Brightness Control System Using First Order Sugeno Fuzzy Model | |
| Wahyudi Wahyudi (Departemen Teknik Elektro UNDIP, Indonesia) | 311 |
| Carbon Monoxide Monitoring System based on IoT with Low Power Sensor Node for Indoor Applications | |
| Amalia Nur Hikmah (National Chin-Yi University of Technology, Taiwan, Taiwan), C. Bambang Dwi Kuncoro (National Chin-Yi | |
| University of Technology, Taiwan) | 316 |
| The Fuzzy PID Controller Performance in BLDC Motor Rotor Speed Variable | |
| Nana Sutarna (Politeknik Negeri Jakarta, Indonesia), Bernadeta Purwanti (Politeknik Negeri Jakarta, Indonesia), Lingga Suhadha | |
| (Politeknik Negeri Jakarta, Indonesia) | |

| An integrated model based on the location-based services for Higher Educational Systems LBS-HES | |
|---|-----|
| Ahmed Alshaflut (IT, Saudi Arabia) | |
| Analysis Perceptions Regarding Student Exchange Using Simple Random Sampling and AHP Methods | |
| Orissa Octaria (University of Multi Data Palembang & Satya Wacana Christian University, Indonesia), Kristoko Dwi Hartomo | |
| (Universitas Kristen Satya Wacana, Indonesia), Irwan Sembiring (Universitas Kristen Satya Wacana Salatiga, Indonesia), | |
| Hindriyanto D Purnomo (Satya Wacana Christian University, Indonesia), Ade Iriani (Satya Wacana Christian University, | |
| Indonesia), Eko Sediyono (Universitas Kristen Satya Wacana, Indonesia) | 331 |
| People Tracking and Re-Identifying in Distributed Contexts: Extension Study of PoseTReID | |
| Ratha Siv (University of Mons, Belgium), Matei Mancas (University of Mons, Belgium), Bernard Gosselin (University of Mons, | |
| Belgium), Dona Valy (Institute of Technology of Cambodia, Cambodia), Sokchenda Sreng (Institute of Technology of Cambodia | |
| (ITC), Cambodia) | 337 |
| Spelling Checking with Deep Learning Model in Analysis of Tweet Data for Word Classification Process | |
| Arif Ridho Lubis (Politeknik Negeri Medan, Indonesia), Mahyuddin K. M. Nasution, yudi (Universitas Sumatera Utara & Fakultas | |
| Ilmu Komputer dan Teknologi Informasi (Fasilkom-TI) USU, Indonesia), Opim Salim Sitompul (Universitas Sumatera Utara, | |
| Indonesia), Elviawaty Muisa Zamzami (Universitas Sumatera Utara, Indonesia) | 343 |
| Sentiment Analysis of Text Memes: A Comparison Among Supervised Machine Learning Methods | |
| Endah Asmawati (Institut Teknologi Sepuluh Nopember & Universitas Surabaya, Indonesia), Ahmad Saikhu (Institut Teknologi | |
| Sepuluh Nopember, Indonesia), Daniel Siahaan (Institut teknologi Sepuluh Nopember, Indonesia) | |
| Ensemble Image Colorization using Convolutional Neural Network | |
| Kriztoper D Urmeneta (University of the Philippines Visayas Tacloban College, Philippines), Victor Romero II (University of the | |
| Philippines, Philippines) | |
| Improving Recommender Systems Performance with Cross-domain Scenario: Anime and Manga Domain Studies | |
| Rizal Broer Bahaweres (UIN Jakarta - IPB University & Computer-iEEE, Indonesia), Ahmad Ruslan Almujaddidi (State Islamic | |
| University Syarif Hidayatullah Jakarta, Indonesia) | |

| Brain Tumor Detection on Magnetic Resonance Imaging (MRI) Images Using Convolutional Neuro | al Network |
|--|--------------------|
| Rarasmaya Indraswari (Institut Teknologi Sepuluh Nopember, Indonesia), Indira Ardan (Institut Teknologi Se | puluh Nopember |
| (ITS), Indonesia), Agus Arifin (Institut Teknologi Sepuluh Nopember Surabaya, Indonesia), Aris Tjahyanto (Sej | puluh Nopember |
| Institute of Technology, Indonesia), Nur Aini Rakhmawati (Institut Teknologi Sepuluh Nopember Surabaya, In | ndonesia), Renny |
| Kusumawardani (Institut Teknologi Sepuluh Nopember (ITS), Indonesia) | |
| Fine-Grained Sentiment Analysis on PeduliLindungi Application Users with Multinomial Naive Ba | yes-SMOTE |
| Imam Suyuti (Universitas Sebelas Maret, Indonesia), Dewi Retno Sari S. (Universitas Sebelas Maret, Indonesia | ⁱ⁾ 374 |
| Sentiment analysis on E-Marketplace User Opinions Using Lexicon-Based and Naïve Bayes Model | ! |
| Safitri Juanita (Universitas Budi Luhur, Indonesia), Krisna Adiyarta (Universitas Budi Luhur, Indonesia), Muhan | nmad Syafrullah |
| (Universitas Budi Luhur, Indonesia) | |
| Extraction of Event Sentence Information in the Covid-19 Distribution Location Detection Syste Indonesian Language Corpus | em based on the |
| Erwin E (Universitas Sriwijaya, Indonesia), Fathoni Fathoni (Universitas Sriwijaya, Indonesia), Abdiansah Abdia | ınsah (Universitas |
| Sriwijaya, Indonesia) | |
| Hops Plants Disease Detection using Feature Selection based BPSO-SVM | |
| Athiyyatul Farhanah (Telkom University, Indonesia), Wikky Fawwaz Al Maki (Telkom University, Indonesia) | |
| Analysis of Job Placement Based on Employee Competency Using Profile Matching | |
| Hari Soetanto (Universitas Budi Luhur, Indonesia), Painem Painem (Universitas Budi Luhur, Indonesia), Utomo | o Budiyanto (Budi |
| Luhur University, Indonesia) | |
| | |

Compact MIMO Antenna Array for 5G Applications Sabah Ghadeer (Universiti Teknologi Malaysia (UTM), Iraq), Sharul Kamal A. Rahim (Universiti Teknologi Malaysia, Malaysia), Taha Elwi (UPM, Malaysia) Large Scale Lightning Electromagnetic Interference to 4G Mobile Communication Network Muhammad Ammar Jamal Akbar (Universiti Teknikal Malaysia Melaka, Malaysia), Mohd Riduan Ahmad (Universiti Teknikal Malaysia Melaka, Malaysia), Shamsul Ammar Shamsul Baharin (Universiti Teknikal Malaysia Melaka, Malaysia), Mardina Abdullah (Universiti Kebangsaan Malaysia, Malaysia), Mohamad Zoinol Abidin Bin Abd Aziz (Universiti Teknikal Malaysia Melaka & Hang Tuah Jaya, Malaysia), Gaopeng Lu (University of Science and Technology of China & School of Earth and Space Sciences, China) 403 Development of Autonomous Control System using Self-Organizing Map and Autoregressive Self-Organizing Map Agila Dzikra Ayu (Universitas Indonesia, Indonesia), Hansel Matthew (Universitas Indonesia, Indonesia), Iman Herlambang Suherman (Universitas Indonesia, Indonesia), Aries Subiantoro (Universitas Indonesia, Indonesia), Benyamin Kusumoputro (Universitas Indonesia, Indonesia) 407 Design and Analysis of Multi-Core Fiber with SDM (Space Division Multiplex) Technology in Singapore to Surabaya via Southern Sea of Java Tri Kushartadi (University of Indonesia, Indonesia), Teuku Rafi (Universitas Indonesia, Indonesia), Akhmad Sarif (Universitas On the Performance of a Composite Right Left Hand Electromagnetic Bandgap Structure Rana Riad Al-Taie (AL-Mustansiriya University, Iraq), Mustafa Mahdi Ali (Mustansiriyah University, Iraq & Iraqi Engineering Union, unknown), Yasir Al-adhami (Al-Turath University, Iraq), Hind Salim Ghazi Action (Al- Turath University College Computer Engineering, Irag), Noor Noori (Universiti Putra Malaysia, Malaysia), Taha Elwi (UPM, Malaysia) Triple band fractal based on T stub waveguide for sub-6 of 5G Ahmed Raed Al-Tameemi (Al-Nisour University College, Iraq), Goh Chin Hock (Universiti Tenaga Nasional, Malaysia), Taha Elwi (UPM, Malaysia), Taha Raad Al-Shaikhli (Al-Nisour University College, Iraq), Jamal Kamil Kh. Abbas (Al-Nisour University College, Iraq), Bashar Sami Bashar (Al-Nisour University College, Iraq), Mohammed Abed Jawad (Al-Nisour University College, Iraq) 424 Stock Prediction of Multivariable Using Bi-Long Short Term Memory and Capsule Neural Network Ade Ridwan Nugraha (Universitas Jenderal Ahmad Yani, Indonesia), Esmeralda Contessa Djamal (Universitas Jenderal Achmad

| Meta-Heuristic Algorithm to Research on Path Planning Problem of Optical Fiber Transmission Network | |
|---|-----|
| Suhad Qasim (University of Al- Nahrine, Iraq), Noor ALfaisaly (AL Nahrain University, Iraq), Ammar Ibrahim Majeed (Al-Nahrain University, Iraq) | 435 |
| Wifi-6 Antenna Design to Increase Data Traffic Offloading with HFSS and PCAAD Software | |
| Ruliyanta Ruliyanta (Universiti Teknikal Malaysia Malaka, FKEKK JI. Durian Tunggal Ayer Keroh Malaka & Universitas Nasional, Jakarta, Indonesia), Mohd Riduan Ahmad (Universiti Teknikal Malaysia Melaka, Malaysia), Azmi Awang Md Isa (Universiti Teknikal Malaysia Melaka, Malaysia), Viktor Vekky Ronald Repi (Universitas Nasional, Indonesia) | 441 |
| A Novel Conformal MIMO Antenna Array based a Cylindrical Configuration for 5G Applications | |
| Ahmed Raed Al-Tameemi (Al-Nisour University College, Iraq), Taha Elwi (UPM, Malaysia), Goh Chin Hock (Universiti Tenaga Nasional, Malaysia), Taha Raad Al-Shaikhli (Al-Nisour University College, Iraq), Bashar Sami Bashar (Al-Nisour University College, Iraq), Mohammed Abed Jawad (Al-Nisour University College, Iraq), Jamal Kamil Kh. Abbas (Al-Nisour University | |
| College, Iraq) | 446 |
| An Investigation of Ultrashort Pulses Propagation in Atmospheric Turbulence of FSO Communications | |
| Ucuk Darusalam (Universitas Nasional, Indonesia), Purnomo Sidi Priambodo (Universitas Indonesia, Indonesia) | 452 |
| Optimizing Detection Using Multiple Threshold to Combat Low SNR Regime in CRN Arief Marwanto (Universitas Islam Sultan Agung (UNISSULA) Semarang, Indonesia), Haikal Satria (Universiti Teknologi Malaysia, | |
| Malaysia), Sharifah Kamilah Syed Yusof (Universiti Teknologi Malaysia, Malaysia) | 457 |

Construction of Slow and Fast Field Antenna for Detecting Lightning Strikes in South Sumatera

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Abstract— Two antennas - a slow-field antenna and a fastfield antenna - are constructed to measure the electric field generated by lightning. A 50-ohm RG-58 coaxial cable connects each antenna to a high-speed buffer circuit. The OPA633 is utilized in both buffer circuits, which have identical designs. The only difference between the two buffer circuits is the buffer capacitance value, which is 15 pF for the fast field and 10 nF for the slow field. The electric field measured by this circuit represents the electric field strength normal to the ground. Both buffer circuits function well up to frequencies of 100 kHz for the slow field and 1 MHz for the fast field, according to the test findings and circuit simulation with NI MULTISIM 13.0. This measuring equipment has successfully captured electromagnetic waves from lightning with noise levels as low as 180 mV.

Keywords—slow field, fast field, buffer circuit, parallel plate antenna, lightning detection

I. INTRODUCTION

Lightning is a very complex discharge process that emits energy and electromagnetic radiation. Lightning occurs when two different regions of the atmosphere receive a charge large enough to produce an electric field. The increase in the electric field turns the air into a conductor. As a result, the lightning channel acts as an effective transmitting antenna for electromagnetic waves over a wide frequency range from ULF to VHF [1]. The lightning strike is an atmospheric discharge phenomenon regarded as one of the world's most severe natural disasters. This discharge can harm living beings or buildings directly or indirectly through induced currents that result in a rise in electric potential between one or more sites of contact. Forest fires, building damage, disruption to various electronic and telecommunications systems, damage to electrical power systems, and harm or death to humans and animals were examples of physical impairment [2]-[4]. This reason is the fundamental foundation of lightning protection.

Cloud-to-ground (CG) lightning is one of the four types of lightning that causes the most damage to people, facilities, structures, and equipment [5]. One of the most often used approaches for studying and characterizing the features of CG lightning flashes – such as current amplitude, current derivative, polarity, multiplicity, and total flash duration – was indirect lightning measurement. It utilized sensors and remote devices to capture the emitted electric fields formed during the discharge. These measurements led to the identification of several features of the CG flash that were important for formulating lightning protection standards and establishing a lightning warning network and localization system.

One feasible way for researchers to measure electric fields was to use two parallel plate antennas with identical characteristics [6]–[11] separated by a distance known as the baseline. Lightning electromagnetic radiations propagate vertically throughout all directions from the discharge channel, where they are recognized and recorded by the parallel plate antenna. Different field signatures are sensed by this antenna, which is linked to an electrical circuit through a coaxial cable. Lightning generates electric and magnetic field signatures recorded by the parallel plate antenna system. Detailed information about the parallel plate antenna system and calibration was found in [12]. This measuring system had some advantages, such as simplicity of implementation, low cost, and excellent capability to provide valuable information [5].

This paper presents the design of a parallel plate antenna and the electronic circuit, which was functioned to detect the intensity of the slow and fast electromagnetic fields generated by lightning discharges in the Southern Equator. The measuring system was installed on the roof of the PTBA Building at the Faculty of Engineering, Sriwijaya University Palembang Campus, South Sumatra. Preliminary findings are also presented in this paper.

II. METHOD

A. Electromagnetic Field Measurement System

The fast and slow electromagnetic fields are measured using two antennas separated by about 2 m. The physical dimensions and design of the antenna were based on research by Galvan and Fernando [12] that was later adjusted by other researchers [13]–[16]. Figures 1 and 2 show the physical features of the antennas used in this study and the configuration of the measuring equipment.

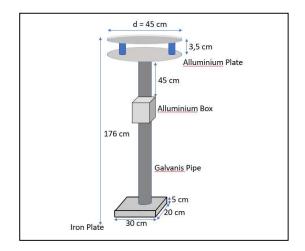


Fig 1. The physical dimensions and design of the antenna used in the study

In principle, any shape may be utilized for the antenna that measures the vertical electric field. The circular antenna is utilized in this study since a circle has no sharp edges like a rectangular shape at which corona may occur at the corner or tapered part, impacting the measurement. The air gap between plates, d, is set to 3.5 cm to keep the capacitance between parallel plates small, according to equation C = (eA)/d. The value of *C* will affect the value of the decay time constant τ_d .

As shown in Figure 2, measurement of changes in the intensity of electromagnetic fields generated during flash is carried out using broadband E-field parallel plate antenna connected to the:

- Buffer circuit as a signal amplifier/buffer in the certain frequency range in the form of : (a) slow-field buffer that works at the frequency of 1Hz-100 kHz to record static components and induction changes in electromagnetic fields from lightning strikes that occur at a radius of less than 30 km from the observation station [17]; (b) fast-field buffers are used to record the activity of electromagnetic radiation fields with frequencies of 1 Hz – 3 MHz, indicating a series of processes from a series of CG-flashes pulses and also to observe amplitude and rise time values.
- 2. Picoscope 5000 series data acquisition device integrated into a PC.

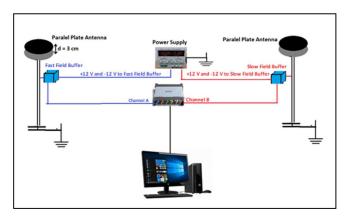


Fig 2. System measurement configuration

The 50- Ω coaxial cable (type RG-58) connects both antennas with a series of buffers. The cable length leading to the fast-field buffer input is 23 cm long, and the slow-field buffer input along 28 cm. Both buffer outputs are connected to a Picoscope 5000 series input using a 6 m long coaxial cable. The fast-field buffer circuit is connected to channel A (CH. A) on a Picoscope, while a slow-field buffer circuit is connected to channel B (CH. B). The equivalent circuit of the measurement system is shown in Fig 3.

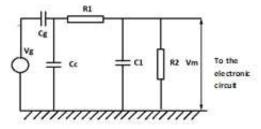


Fig 3. The equivalent circuit of measurement system [12],[18],[19].

The parallel plate antenna has a capacitance of 60.5 pF (Cg). It is connected to the electronic circuit through an RG58 coaxial cable with a capacitance value of 93.5085 pF/m (Cc). Capacitor C1 is an electrical element to measure the voltage change on the antenna plate (Vg). This voltage change is proportional to the electric field change produced by a lightning flash. For the fast field antenna, the value of C1 is 15 pF, while for the slow field is 10 nF. A 50-ohm resistor, R1, is placed at the entry of the electrical circuit to terminate the characteristic impedance of the coaxial cable, which connects the antenna and the electrical circuit. Since the input impedance of the buffer amplifier is very high, resistor R2 is shunted with C1 to extend the decay time constant, R2C1. The value of R2 is 100 MΩ.

A high-speed buffer circuit is required to obtain accurate lightning E-field measurement results. IC OPA 633 KP from Burr Brown was utilized as a high-speed buffer. The IC OPA 633 KP is a high-speed buffer amplifier with monolithic gain with a bandwidth of 260 MHz and a high slew rate (2500 V/ μ s) [20]. Another advantage of this IC is that its high output current capability allows the OPA633 to drive the 50 Ω cable used in our measurement system

B. Calculation of Capacitance Values and Buffer Circuit Initiation Frequency

The first step was calculating the capacitance values of the fast-field buffer circuit and slow field (Cb), the connecting coaxial cable from the antenna to each input buffer circuit buffer (Cc-in), and the connecting coaxial cable from the buffer circuit output buffer to the Picoscope input (Cc-out). The capacitance value of this coaxial cable was determined by its length multiplied by its specific capacitance value. The circuit capacitance value is listed in Table 1.

 TABLE I. THE CAPACITANCE VALUE OF THE ELECTROMAGNETIC FIELD

 Measurement system

 No
 Component
 Capacitance

| No | Component | Capacitance |
|----|--|-------------|
| 1 | Parallel plate antenna, <i>Ca</i> | 60,5 pF |
| 2 | Buffer fast field, <i>C</i> _{ff} | 15 pF |
| 3 | Buffer slow field, <i>C</i> _{sf} | 10 nF |
| 4 | Coaxial cable – input buffer fast field, Cc.in-ff | 21,507 pF |
| 5 | Coaxial cable – input buffer slow field, $C_{c-in-sf}$ | 26,182 pF |
| 6 | Coaxial cable buffer fast field – input Picoscope | 1533.539 pF |
| 7 | Coaxial cable buffer slow field – input Picoscope | 1366.159 pF |

The next step determined each buffer circuit's decay time and the initial frequency response. By using the capacitance values listed in Table 1, it is obtained:

The decay time constant (τ) for fast-field buffer antenna is calculated using Eq. 1.

$$\tau = R. C_T = R. (C_a + C_{c-in-ff} + C_{ff})$$
(1)
$$\tau = (100M\Omega) (60.5 \text{ pF}+21,507 \text{ pF}+15\text{pF})$$

= 9.7007ms

And the decay time constant (τ) antenna for the slow-field buffer is obtained using Eq. 2.

$$\tau = R. C_T = R. \left(C_a + C_{c-in-sf} + C_{sf} \right) \tag{2}$$

 $\tau = (100 \text{M}\Omega)(60.6 \text{ pF}+26,182 \text{ pF}+10 \text{ nF})$ = 1008,2007ms

Those decay time constants are large enough to record lightning-generated electric field signals accurately with reasonable accuracy.

From the value of τ , the initial frequency response (f_o) in the fast-field buffer amplifier circuit is calculated using Eq. 3.

$$f_o = \frac{1}{2\pi\tau} = \frac{1}{2.3,14.(0,0097s)} = 16.4Hz$$
(3)

And for slow-field buffer amplifier circuit is obtained using Eq. 4.

$$f_o = \frac{1}{2\pi\tau} = \frac{1}{2 \cdot 3.14 \cdot (1,0082s)} = 0.16 \ Hz \tag{4}$$

C. Testing of Buffer Circuit

Before being used for actual measurement, the slow and fast field buffer circuits needed to be tested. The arrangement of the measurement circuit is shown in Figure 4. Direct measurements on the buffer circuit were performed by connecting the buffer output to the Chanel A of the Picoscope. And the buffer input was connected to the generator function in the Picoscope device. Two 9 V batteries were used to power the buffer circuit. Then, the circuit was injected with various values of the sine wave frequency. The frequency was set in Picoscope application software on the PC. The frequency response waveform of the buffer circuit will appear on the PC screen.



Fig 4. Buffer test circuit

D. Simulating the system using MULTISIM

The circuit was then simulated using NI MULTISIM 13.0 software to determine the frequency response of the measurement system. Figure 5 depicts the simulation equivalent circuit of a fast-field buffer and a slow-field buffer.

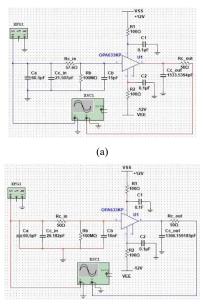




Fig 5. The simulation test circuit of (a) fast filed antenna and (b) slow field antenna $\,$

The electronic components used in this study refer to the previous research[12], [13]. Two high-frequency ceramic capacitors of 0.1 μ F (C1 & C2) were used in both buffer circuits to bypass the power supply connection. They are placed as close as possible to the power supply pins of the buffer for high-frequency decoupling. The 100-ohm resistors R1 & R2 were connected in series with the power supply pins to protect the circuit against damage caused by high currents. The 50-ohm resistor, Rc-out, was placed in series at the output buffer to match the impedance of the circuit to the line's characteristic impedance.

The parameter used to assess circuit performance was the ratio between the input voltage of the buffer circuit (Vm) and the voltage change on the antenna plate (Vg). A buffer circuit filters the frequency spectrum of the lightning flash signal [21] without amplifying it [17]; thus, a suitable buffer circuit has a ratio value close to 1. For simulation, the frequency values tested on both circuits were 1 Hz, 10 Hz, 100 Hz, 1 kHz, 10 kHz, 100 kHz, and 1 MHz, and specifically for fast-field buffer circuits, one test frequency value of 10 MHz was added.

E. Himawari-8 Satellite Cloud Type Imaging

The Himawari-8 geostationary satellites operated by the Japan Meteorological Agency (JMA) support weather forecasting, tropical cyclone tracking, and meteorology research. Most meteorological agencies in East Asia, Southeast Asia, Australia, and New Zealand utilize satellites for their weather monitoring and forecasting operations. One Japanese institution that operates the Himawari-8 data archiving and redistribution service is JAXA (Japan Aerospace Exploration Agency) Himawari Monitor which provides Himawari-8 download system services and data processing (http://www.eorc.jaxa.jp/ptree/index.html).

On the Jaxa Himawari Monitor website, there is a cloudtype option that lists the cloud top pressure and optical thickness measurements made for each cloudy pixel throughout the day. As demonstrated in the figure's color caption section, this information may be used to categorize various types of clouds. The names of the cloud categories used here merely approximate the climatological link between the satellite-measured optical characteristics and the traditional morphological cloud types. Cloud types are indicated by color coding at the bottom of the satellite image, where cumulus clouds are shown in pink.

Additionally, a cloud thickness menu that shows the optical thickness parameter of the cloud at visible wavelengths is available on this page (approximately 0.6 microns). If the cloud equally covers the pixels, the cloud thickness determines the amount of apparent solar reflectivity recorded by the satellite from the cloudy scene. Figure 6 illustrates the association between cloud type and cloud thickness.

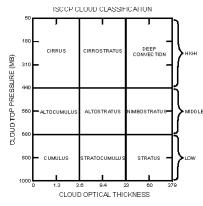


Fig 6. ISCCP Cloud Clasification [21]

III. RESULT AND DISCUSSION

A. Buffer Circuit Performance

The buffer circuit was simulated with NI MULTISIM 13.0 software. The simulation results of the fast-field buffer and slow-field buffer circuits are shown in Figure 7. The result indicates that both buffer circuits have a good response and perform well up to 1 MHz for the fast field and 100 kHz for the slow field. The proposed buffer circuit may therefore be used to measure the E-field produced by lightning.

As previously stated, the buffer circuit is initially evaluated using a generator function to determine how the buffer circuit responds to frequency. Figure 8 demonstrates that both buffer circuits have a good frequency response, shown by frequency response waveforms that are almost pure sinusoidal. The waveform has a little ripple, especially at low frequencies (1 Hz to 100 Hz), although the ripple lessens as the frequency increases. This result demonstrates that the buffer circuit still generates tolerable noise.

This test also measured the voltage, as shown in Table 2. These results indicate that the buffer circuit is functioning well, as indicated by the value of the measuring voltage Vm which is close to the voltage value on the antenna, Vg.

TABLE II. BUFFER VOLTAGE MEASUREMENT

| Buffer Circuit | Frekuensi (Hz) | Vg (V) | Vm(V) |
|-----------------------|----------------|--------|-------|
| Slow-field | 1 | 2,091 | 2 |
| | 10 | 4,041 | 4 |
| | 100 | 4,106 | 4 |
| | 1000 | 4,041 | 4 |
| | 10000 | 4,041 | 4 |
| | 100000 | 3,341 | 4 |
| | 1000000 | 0,6241 | 4 |
| Fast-field | 1 | 2,091 | 2 |
| | 10 | 4,041 | 4 |
| | 100 | 4,041 | 4 |
| | 1000 | 4,041 | 4 |
| | 10000 | 4,041 | 4 |
| | 100000 | 4,041 | 4 |
| | 1000000 | 4,041 | 4 |

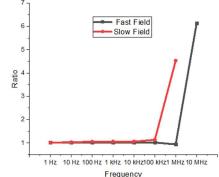


Fig 7. The comparison ratio (Vm/Vg) between slow and fast field buffers

B. Result of Measurement System Field Test

Field tests are the next step to see if the measuring system—the antenna and a buffer circuit—delivers accurate E-field measuring. The measuring system is located on top of the PTBA Building (-3° 22' 13.87",103° 42' 37.14"), Faculty of Engineering Sriwijaya University, Palembang Campus, which has a height of 9.17 m from ground level.

The Picoscope display was configured as follows to obtain the measurement of E-field emission, particularly the return stroke wave :

| - | Recording time | : 500 ms |
|---|-------------------------|--------------------------|
| - | Number of samples | : 10 MS. |
| - | Hardware resolution | : 12 bit |
| - | Trigger Mode | : single |
| - | Coupling mode | : AC. |
| - | Voltage range channel A | $\pm 5V$ (fast field) |
| - | Voltage range channel B | $\pm 2V$ (slow field) |
| - | Pre-trigger time | : 20% |
| - | Trigger level | : 2V for channel A (fast |
| | field) | |

The recording time, the number of samples, hardware resolution, and pre-trigger time are based on prior studies [22]–[24]. The system managed to capture a return stroke of lightning E-field waves on 8 June 2022, as shown in Figure 9. The 180 mV range of noise is still present in the collected waves for both antennas, but it is tolerable.

The return stroke wave taken by the fast field antenna is shown in Figure 9 as a blue line, while the return stroke wave captured by the slow field antenna is shown as a red line. The waveform changes of both antennas co-occurred, indicating that the RS wave captured by the measurement system was within a radius of 30 km from the station.

| Frequency | Buffer Circuit Testing Slow Filed Buffer | Result Fast Field Buffer |
|-----------|--|------------------------------------|
| 1 Hz | | |
| 10 Hz | | |
| 100 Hz | | |
| 1 kHz | | |
| 10 kHz | | |

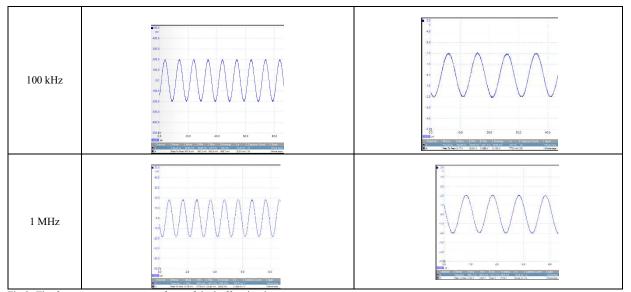
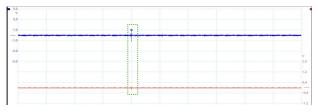
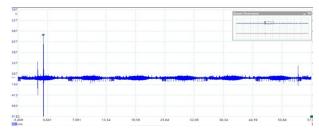


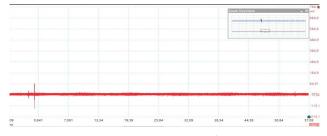
Fig 8. The frequency response waveform of the buffer circuit



(a) Lightning E-field in slow and fast field buffer on June 8th, 2022



(b) Enlarged image of fast field wave on June 8th, 2022



(c) Enlarged image of slow field wave on June 8th, 2022

The captured waveform resembles the return stroke (RS) wave observed in several other areas, such as Malaysia and Sweden [25] and Padang, West Sumatra [24], as shown in

Figure 10. RS waves are characterized by sudden high spikes on the microsecond and sub-microsecond timescales [26].

The data from sensors were also confirmed by comparing the changes in the electric field recorded by the measurement system with the Himawari-8 IR-enhanced satellite imaging results. The image showed lightning flash occurrences accompanied by lightning cloud activity (cumulonimbus) in the Palembang region, as shown in Figure 11. The cumulus cloud activity in the Palembang region appeared on June 8th, 2022 at 01.00 UTC (08.00 WIB), as shown in the Himawari satellite image. This image indicated that lightning activity occurred simultaneously with the detected waves.

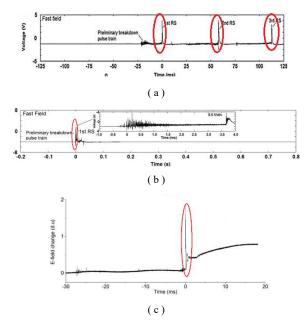


Fig 10. Examples of return stroke waveforms taken during a thunderstorm in (a) Malaysia, (b) Sweden, and (c) Padang,West Sumatera [24], [25].

Fig 9. Lighting E-field recorded by the proposed measurement system



Fig 11. JAXA Himawari Monitor's cloud-type for the Palembang area at 01.00 UTC on June 8th, 2022

IV. CONCLUSION

The developed system has proven capable of receiving and recording the lightning-generated electric fields on June 2022 in Palembang, South Sumatra. Since this system is also meant to be a lightning locating system in South Sumatra, the study described in this paper still needs development and improvement. Further works will involve creating a VHF antenna to complement the current system and formulating a mathematical model for signal pre-processing based on the South Sumatra lightning emission signal characteristics to improve lightning strike location detection.

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